

Experimentally detecting and mitigating trapped flux at NIST

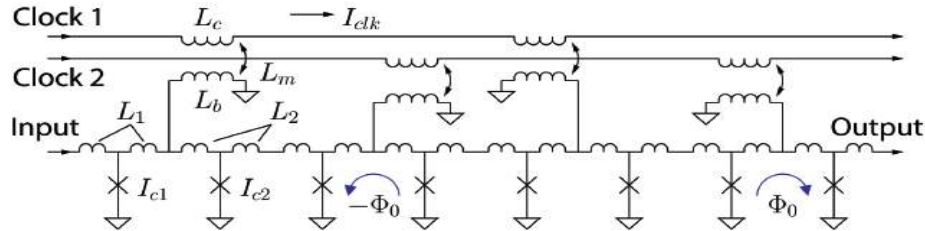
Presenter: Pete Hopkins
Superconductive Electronics Group

Superconductive Electronics Group



Why is trapped flux bad for SFQ logic?

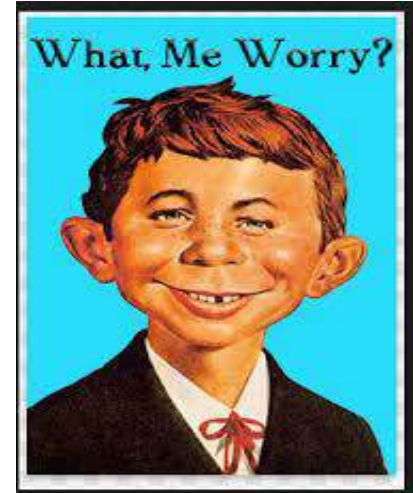
SFQ Circuits are based on Single Flux Quanta signals



Trapped flux are one or more single flux quanta

Fluxons trapped in circuits produce lower operating margins and/or nonfunctional circuits.

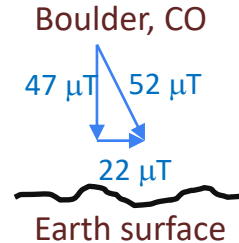
- Phase shift in JJs and SQUIDs
- Alters the bias of circuits



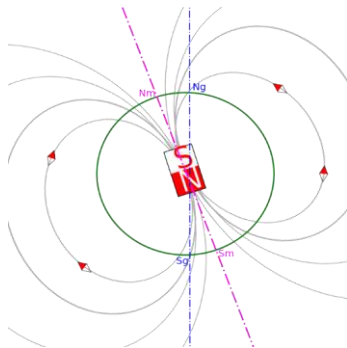
Magnitude and direction of Earth's field

http://en.wikipedia.org/wiki/Earth's_magnetic_field

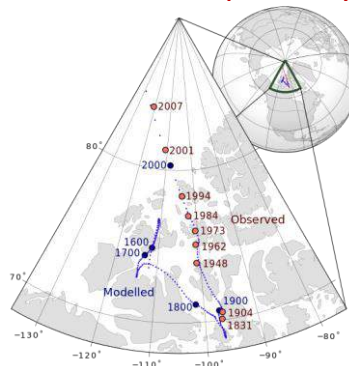
1. Source: geodynamo -> motion of molten iron alloys in outer core
2. Acts to deflect Solar Wind (charged particles that would carry away the Ozone, etc.)
3. Magnitude: 25-65 μT surface (highest near the poles, lowest near equator)
 - $\sim 52 \mu\text{T}$ (Boulder) http://upload.wikimedia.org/wikipedia/commons/c/c7/WMM2010_F_MERC.pdf
4. Direction: Straight down/up at N/S poles, horizontal at equator
 - ~ 65 degrees inclination (surface), ~ 10 deg declination (NEast) at Boulder
 - http://en.wikipedia.org/wiki/File:World_Magnetic_Inclination_2010.pdf
 - http://en.wikipedia.org/wiki/File:World_Magnetic_Declination_2010.pdf
5. Reverses at irregular intervals, averaging several x 100k years
6. N & S poles wander independently; not directly opposite



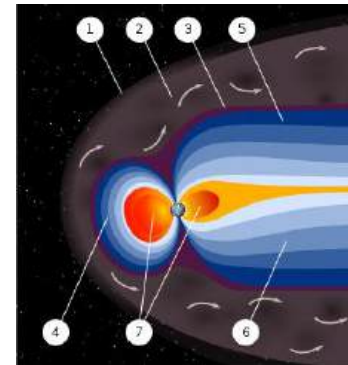
Dipole Approximation



Movement of N pole vs year



Magnetosphere

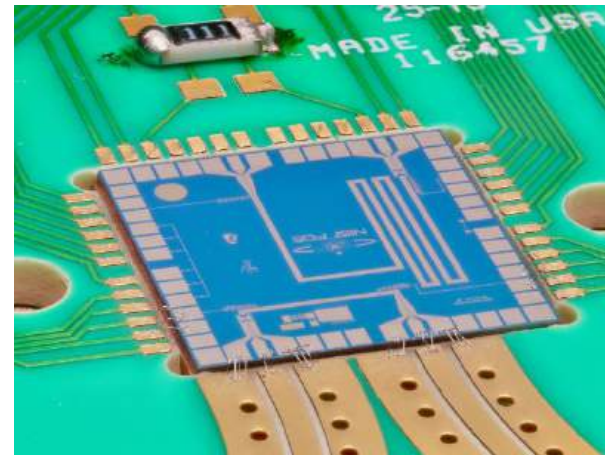


General guidelines

1. Best practices from previous US digital programs
2. Literature list
3. Simulation/measurement example from SuperTools

NIST-specific practices

1. Circuit design
2. Simulation
3. Fabrication
4. Cryostat design and shielding
5. Measurement protocols



Q: What level of (perp.) magnetic flux density B can we tolerate at chip level?

Answer: Must have no trapped flux within circuits

Practical Answer: Mitigation strategies

1. **Reduce ambient field at chip by 100X** (from $\sim 50 \mu\text{T}$ field to $\sim 500 \text{ nT}$).

- Passive mu-metal shielding or passive + active field cancellation

2. **Cell design strategy: 1 trapped flux quantum per moat (max)**

- For 500 nT: 1 flux quantum per $64 \mu\text{m} \times 64 \mu\text{m}$ cell size
- 2-4 border moats per unit cell, moat size follows simple design rules
- Option: ground plane wire lattice

3. **Holistic FAB approach for the full 8 or 10-metal layer stack**

Engineer the master ground plane: T_C and vortex freezing/pinning temp T_f

- Highest T_C and T_f by $> \sim 0.1 \text{ K}$
- Low density of unintentional pinning centers (large $\Delta T = T_C - T_f$ value).
- Not used for carrying high currents (which generate magnetic fields).
- Moat alignment / 2nd ground plane strategy

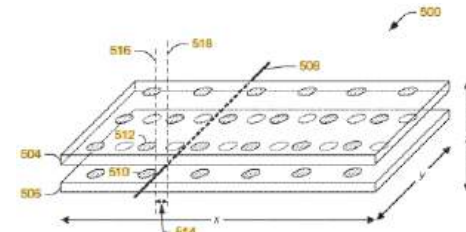


FIG. 5

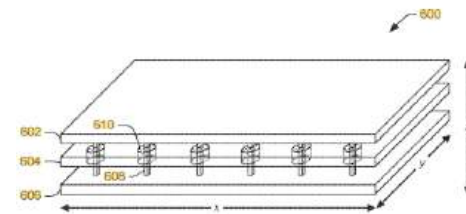


FIG. 6

US Patent: US20200287118A1
Northrop Grumman, 2022

A. Herr et al.

Best practices from US digital programs (2016)

Q: What level of magnetic flux density B can we tolerate at chip level?

Answer: Must have no trapped flux within circuits

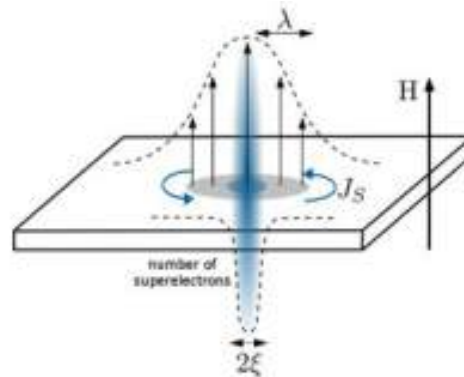
Practical Answer: Mitigation strategies

4. **“Move” the flux quanta before they freeze in place**

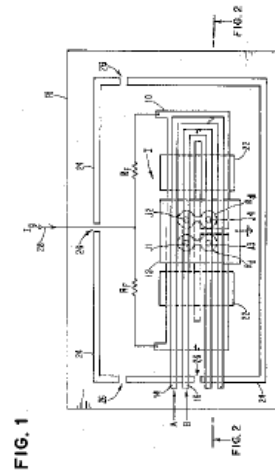
- e.g. use moats or segmented ground planes
- Cool slowly through T_c (~ 1 mK/s)

5. **Add no additional field when $T < T_c$**

- Avoid high current densities, etc.
- Multiple thermal cycles to verify performance (min of 3)



U.S. Patent Jul. 5, 1983 Sheet 1 of 2 4,392,148



US4392148 A Patent
IBM, 1983
Wen H. Chang et al.

Q: Do we need better design tools, supporting data, and procedures for mitigating flux trapping?

A: Yes! Design tools are non-existent; moat design immature; measurement procedures are empirical

Practical Answer

1. Need simulation EDA tools: This could be part of SuperTools.

- Jackman and Fourie 2016 IEEE Trans. Appl. Supercond. 26 1–5

2. Need model-to-hardware correlation to evaluate moat geometry, size, placement, #, etc.

- Fourie and Jackman publications (2016-)
- Circuits with large input currents? speculate that these require unique moat designs.

3. Measurement procedures are empirical

- Cool slowly through T_c (~ 1 -10 mK/s)
- Limiting current on bias lines for circuits requiring large input currents

Reviews:

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2. G. Stan, S. B. Field, and J. M. Martinis, "Critical Field for Complete Vortex Expulsion from Narrow Superconducting Strips," *Physical Review Letters*, vol. 92, no. 9, p. 097003, Mar. 2004. <http://link.aps.org/doi/10.1103/PhysRevLett.92.097003>
3. Y. Polyakov, S. . Narayana, and V. K. Semenov, "Flux Trapping in Superconducting Circuits," *IEEE Transactions on Applied Superconductivity*, vol. 17, no. 2, pp. 520–525, 2007. <http://ieeexplore.ieee.org/lpdocs/epic03/wrapper.htm?arnumber=4277667>
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13. V. K. Semenov, Y. A. Polyakov, and S. K. Tolpygo, "New AC-Powered SFQ Digital Circuits," *IEEE Transactions on Applied Superconductivity*, vol. 25, no. 3, pp. 1–7, Jun. 2015. DOI: 10.1109/TASC.2014.2382665
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Critical field in superconducting Nb strips

G. Stan, S. B. Field, and J. M. Martinis, "Critical Field for Complete Vortex Expulsion from Narrow Superconducting Strips," *Physical Review Letters*, vol. 92, no. 9, p. 097003 Mar 2004 <http://link.aps.org/doi/10.1103/PhysRevLett.92.097003>

Opposing forces: Image force (expel flux) vs. Flux/Meisner currents (push flux to center)

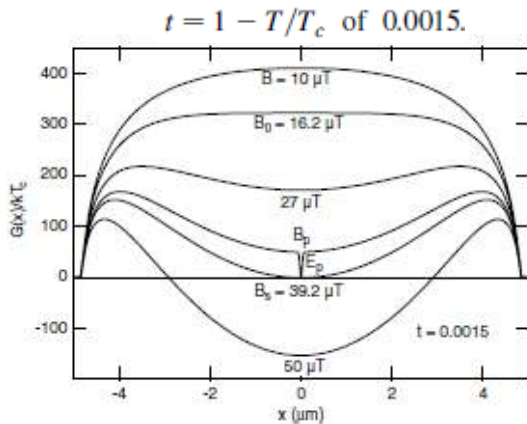
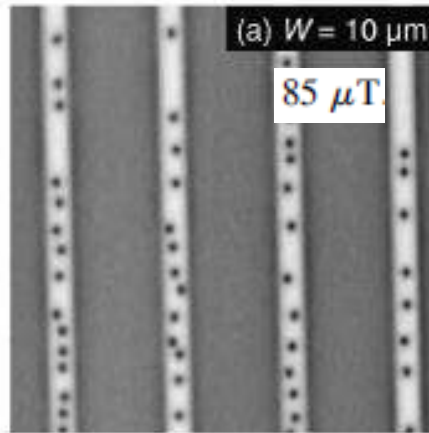
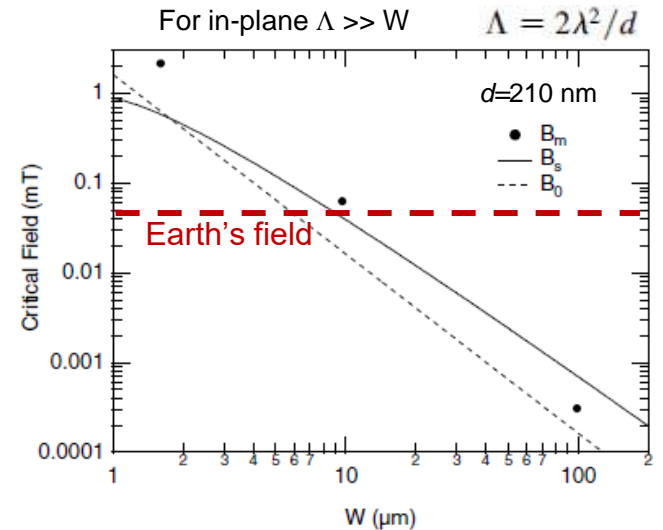


FIG. 1. The Gibbs free energy (Ref. [2]) of a single vortex located at position x at several values of the applied field B , at a reduced temperature $t = 1 - T/T_c$ of 0.0015. The curve at $B_p = 36 \mu\text{T}$ includes schematically a pinning well of depth $E_p \approx 50 kT_c$.



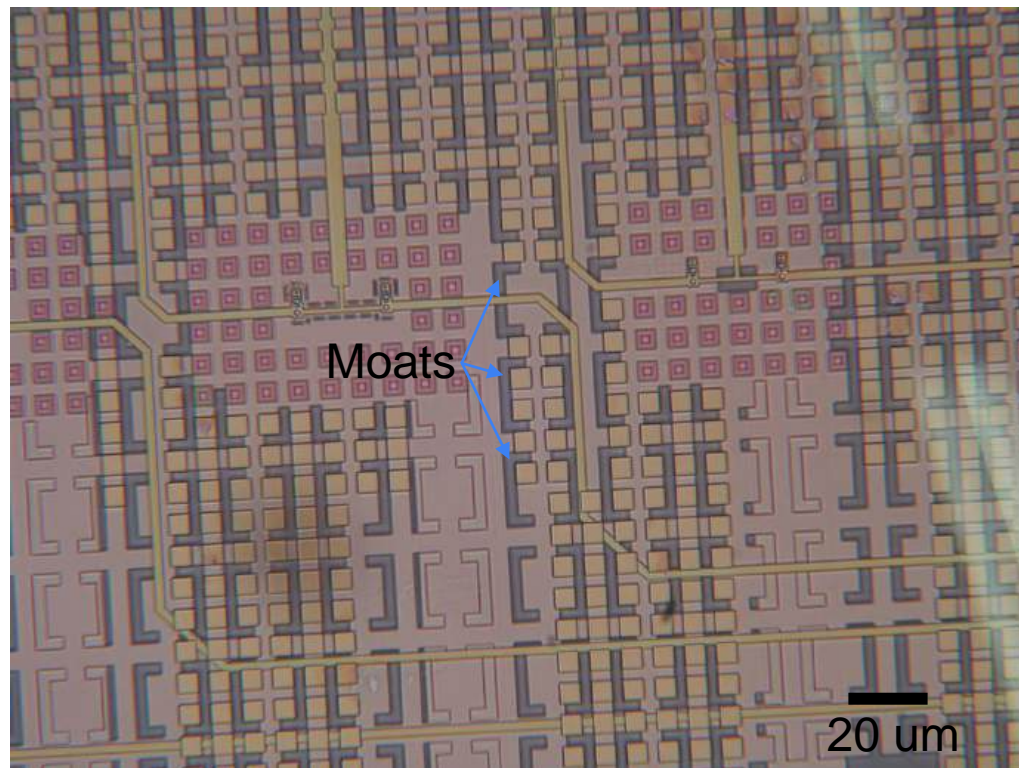
$$B_m \approx \Phi_0 / W^2.$$



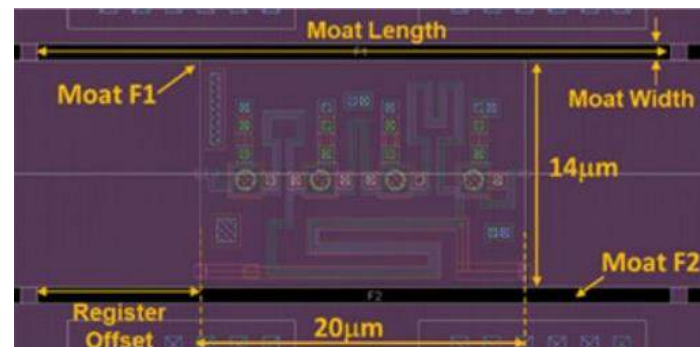
Conclusions:

Universal: Independent of SC materials parameters (if $\Lambda(T_f) \gg W$)
 Design: use narrow wires, avoid large ground planes if possible

Examples of moat designs



Moats divide GP into 14 μm strips



Meninger and Tolpygo (2024)
<https://arxiv.org/pdf/2411.02749>

Under IARPA SuperTools programme (ColdFlux project), we designed a set of flux linkage experiments³.

- Design: SU Fab: MIT-LL Test: NIST

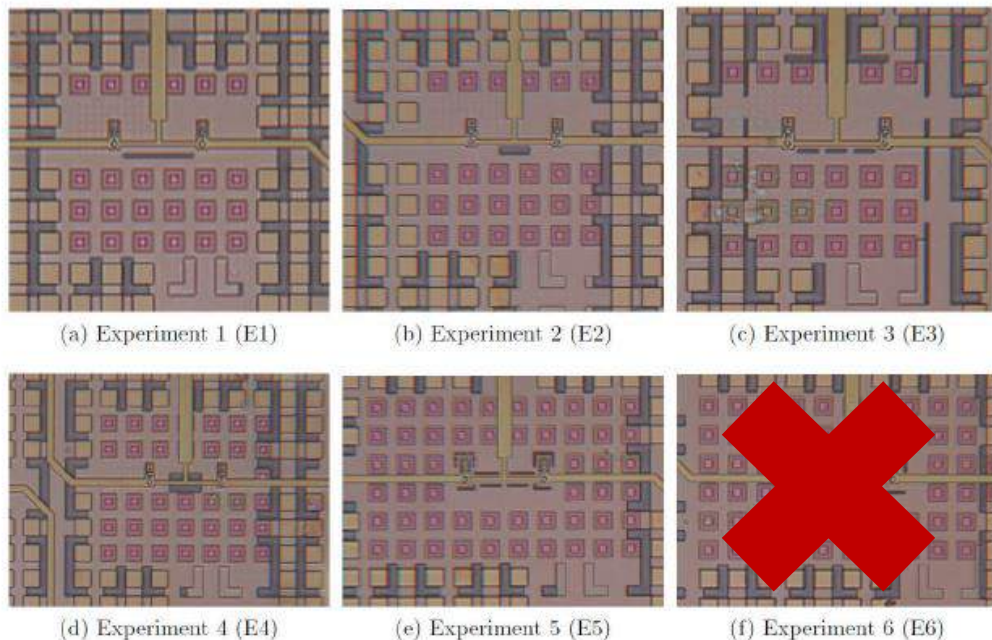


Figure: SQUID test structures

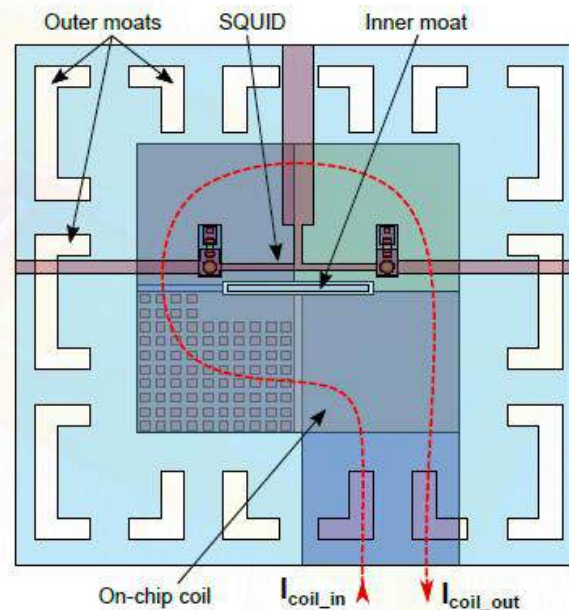


Figure: Configuration of on-chip field coil

³K. Jackman and C. J. Fourie. "Flux trapping experiments to verify simulation models". In: *Supercond. Sci. Technol.* 33 (Aug. 2020), p. 105001.

NIST data from Fourie and Jackman (IEEE TAS 2021)

C. J. Fourie and K. Jackman, "Experimental Verification of Moat Design and Flux Trapping Analysis," *IEEE TAS (2021)* doi: 10.1109/TASC.2021.3051582.

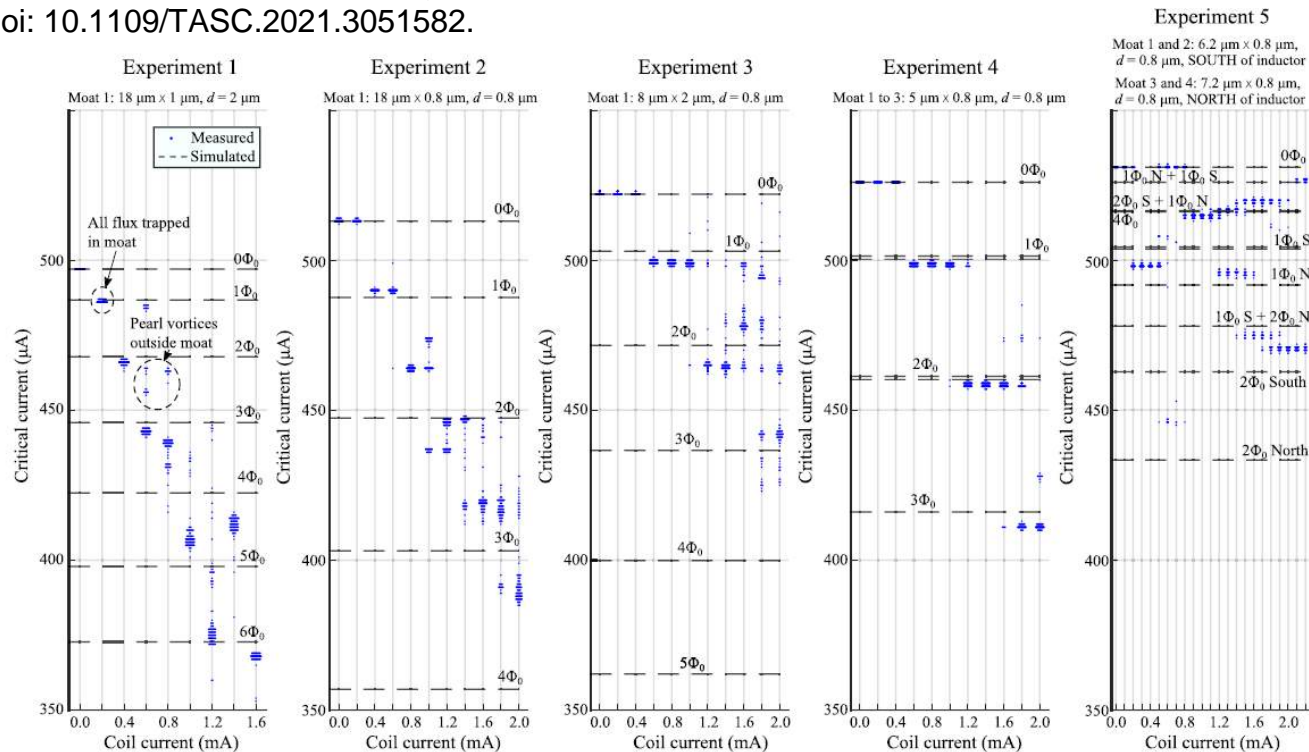
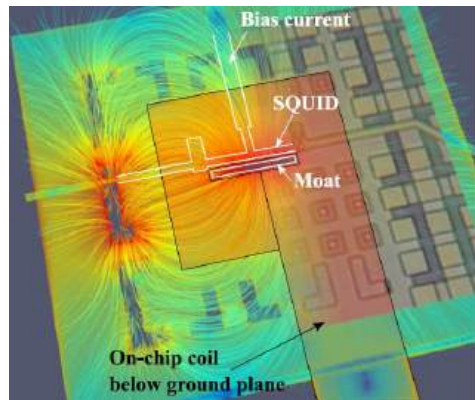


Fig. 9. Critical current of SQUIDs in flux linkage experiments. All simulated trapped flux used flux return path around the edge of the chip.

Data from Manuel Castellanos-Beltran and Adam Sirois, NIST

Compact circuit models for modeling coupling from fluxons in moats to circuit structures have been verified through flux linkage experiments.

With these models, moats can be analysed directly from layouts.

Some conclusions from results:

- Always place more moats than fluxon density per area.
- Double trapping in any moat unlikely for uniform field - Pearl vortices.
- Moats should not run parallel along entire length of an inductor.
- Several staggered moats on opposite sides of inductor (subtract coupling current) better than one long moat.
- Better if moats place perpendicularly to inductors.
- Sky plane with match moats to ground significantly reduces fluxon coupling.

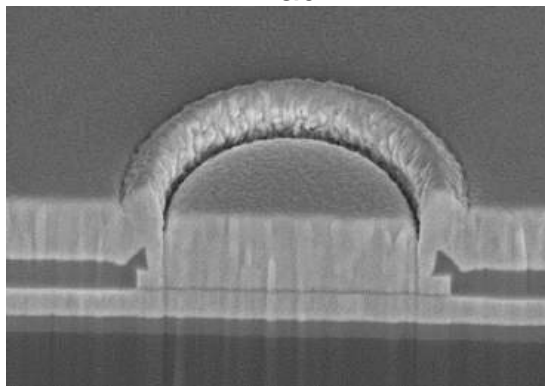
General guidelines

1. Literature
2. Best practices from previous US digital programs
3. Simulation/measurement example from SuperTools

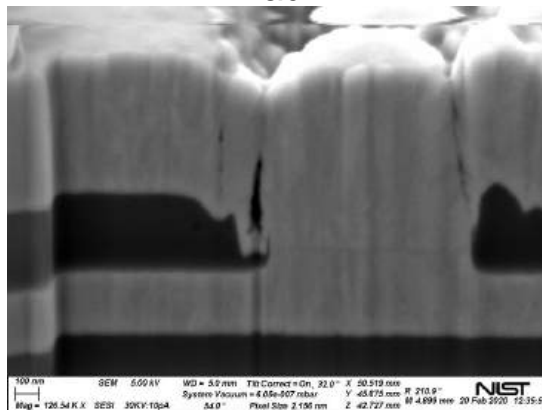
NIST-specific practices

1. Design (no continuous ground planes)
2. Simulation (not presently done)
3. Fabrication
4. Cryostat design and shielding
5. Measurement protocols

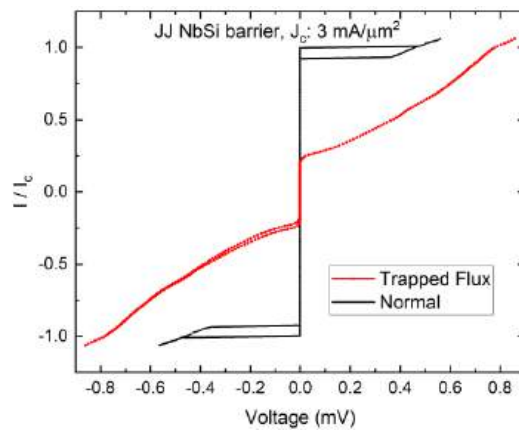
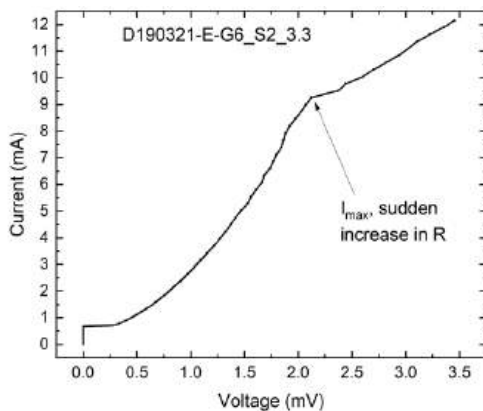
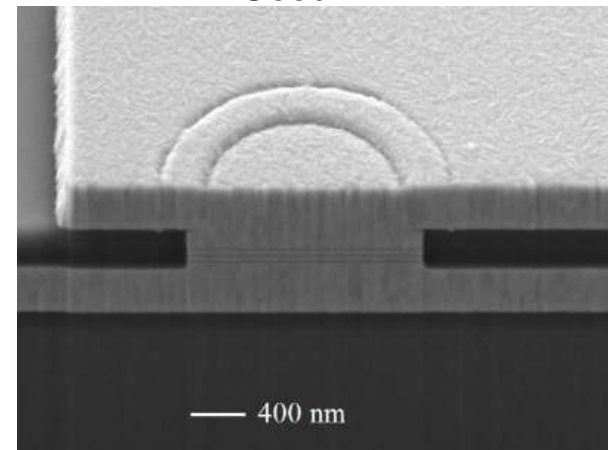
Bad



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Good



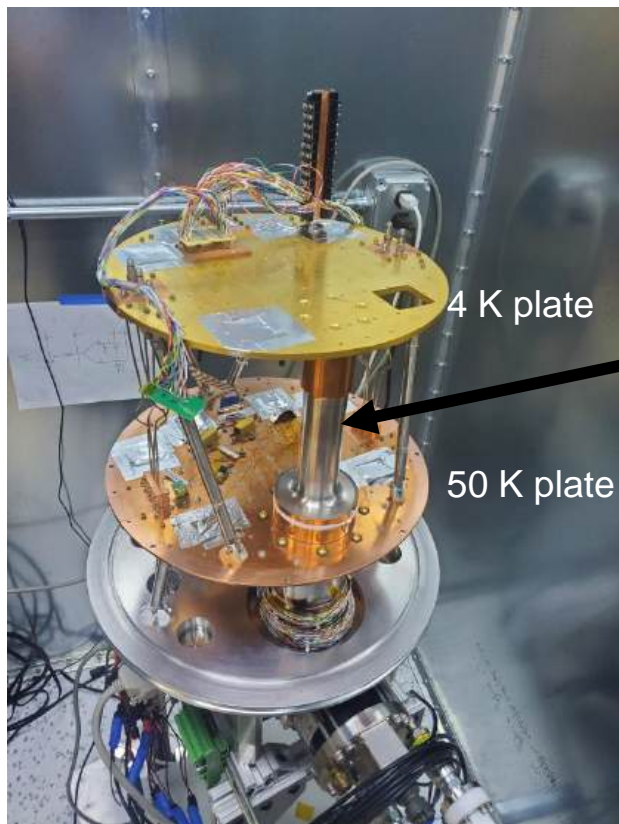
Immersion Probes



- Ni flash for gold plating of components
- De-Gaussed passive mu-metal shields (Length/dia > 4)
- Non-magnetic stainless LHe dewar – watch weld joints!
- Active field cancellation: Helmholtz coil on dewar



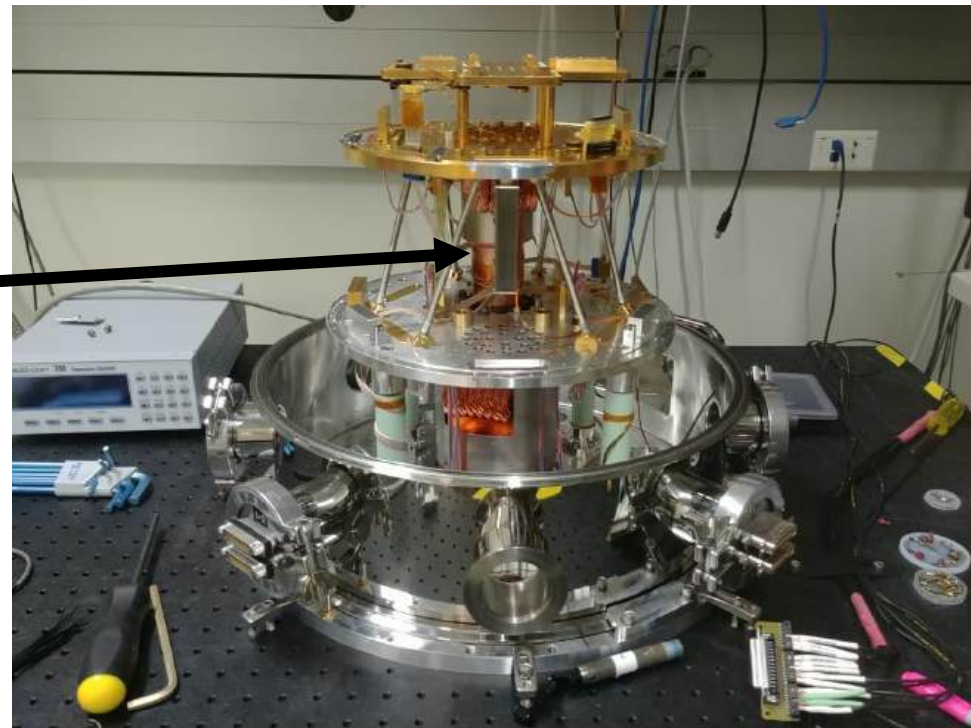
SC Group: Closed-cycle cryostats



4 K plate

50 K plate

2nd Stage
Regenerator



B(t) from 2nd Stage Regenerator

GM Cryocooler

S. Fujimoto et al., *Cryogenics* 35 (1995)

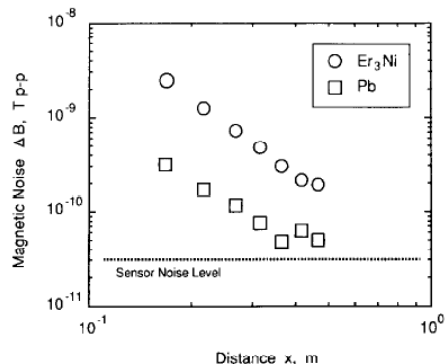


Figure 2 Distance x versus magnetic noise ΔB for the flux-gate magnetometer

Cryogen-free variable temperature scanning SQUID microscope

Cite as: *Rev. Sci. Instrum.* 90, 063705 (2019); doi:10.1063/1.5085008
 Submitted: 7 December 2018 - Accepted: 27 February 2019 -
 Published Online: 25 June 2019



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Pulse Tube

M.J. Eshraghi et al./*Cryogenics* 49 (2009) 334–339

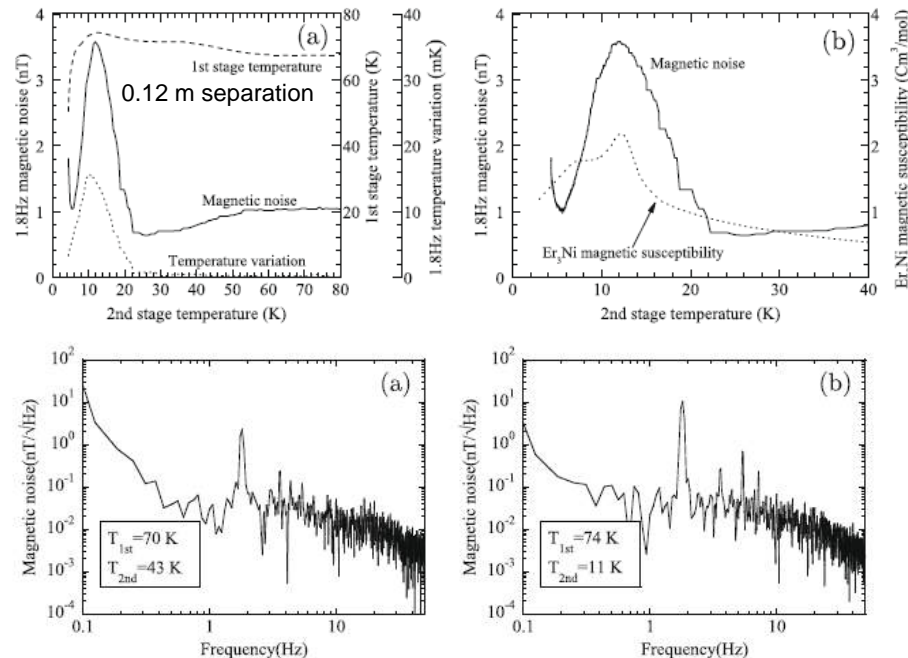
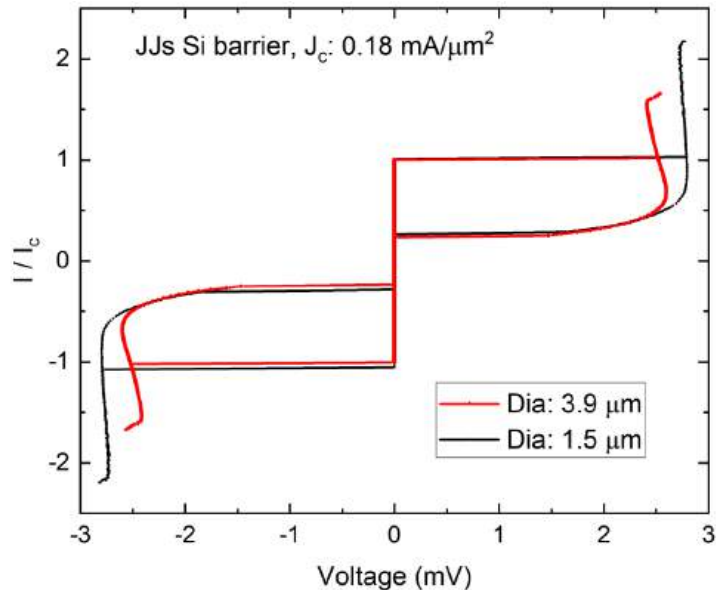
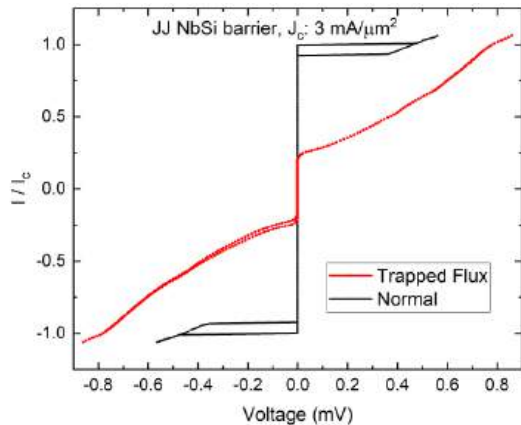
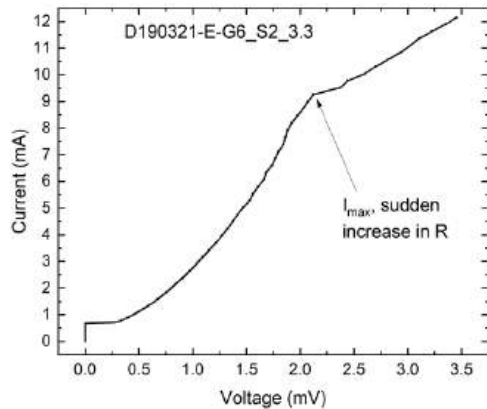


Fig. 3. Magnetic noise spectrum measured by fluxgate magnetometer (a) $T_{2nd} = 43$ K (b) $T_{2nd} = 11$ K.

- Er_3Ni or $HoCu_2$: paramagnetic to antiferromagnetic transition at $T \leq 10$ K.
- Noise source: Temp oscillations + Temperature-dependent magnetic susceptibility



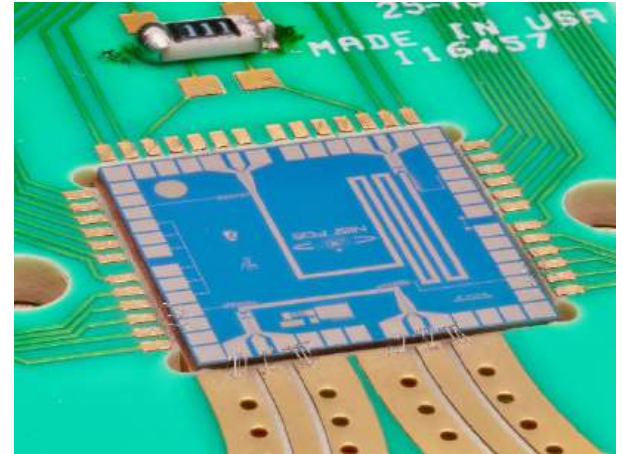
- Testing at high current leads to heating (previously shown)
- Back-bending at gap voltage
- Indicative of sample heating (high I_c)

General guidelines

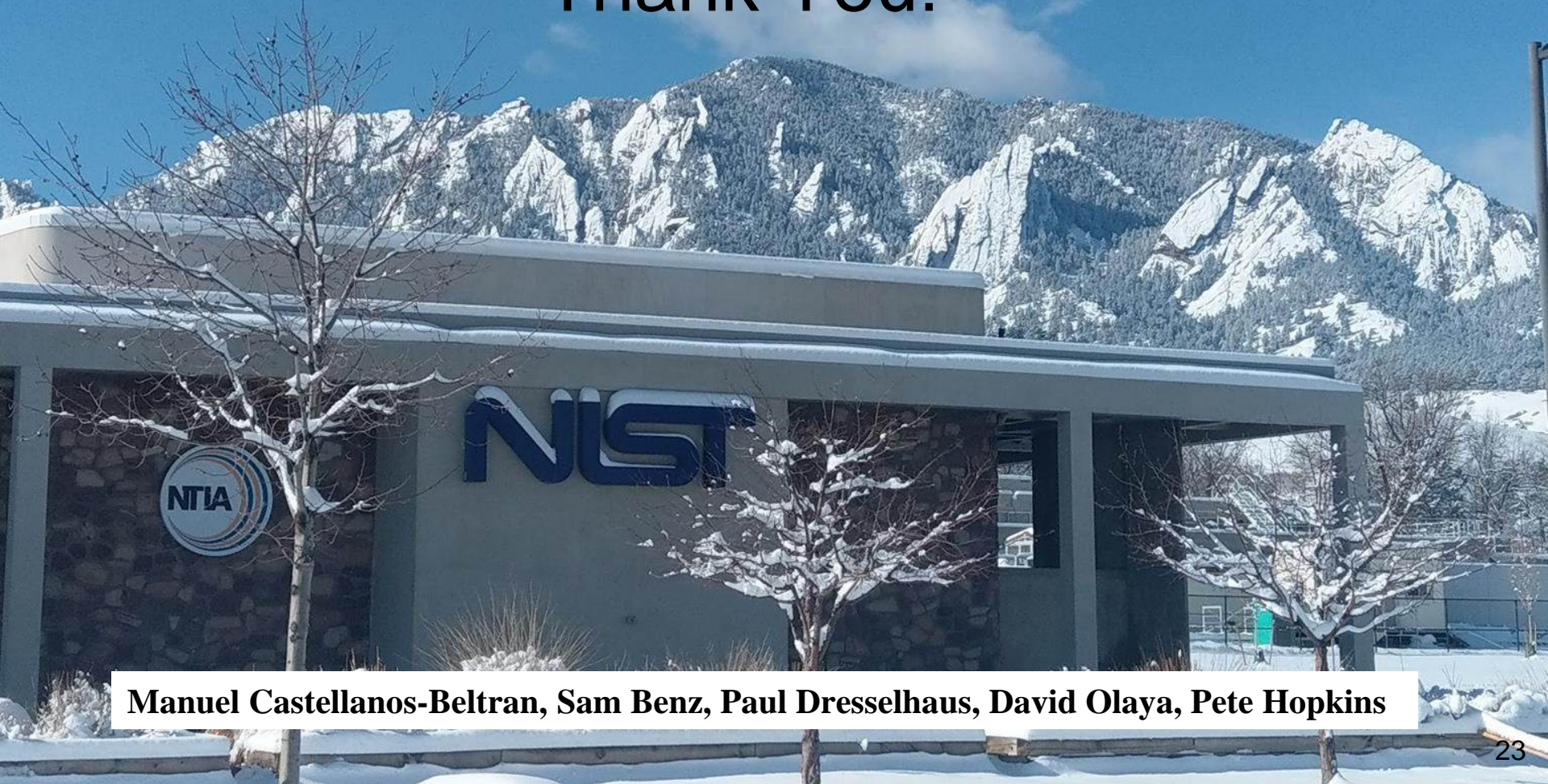
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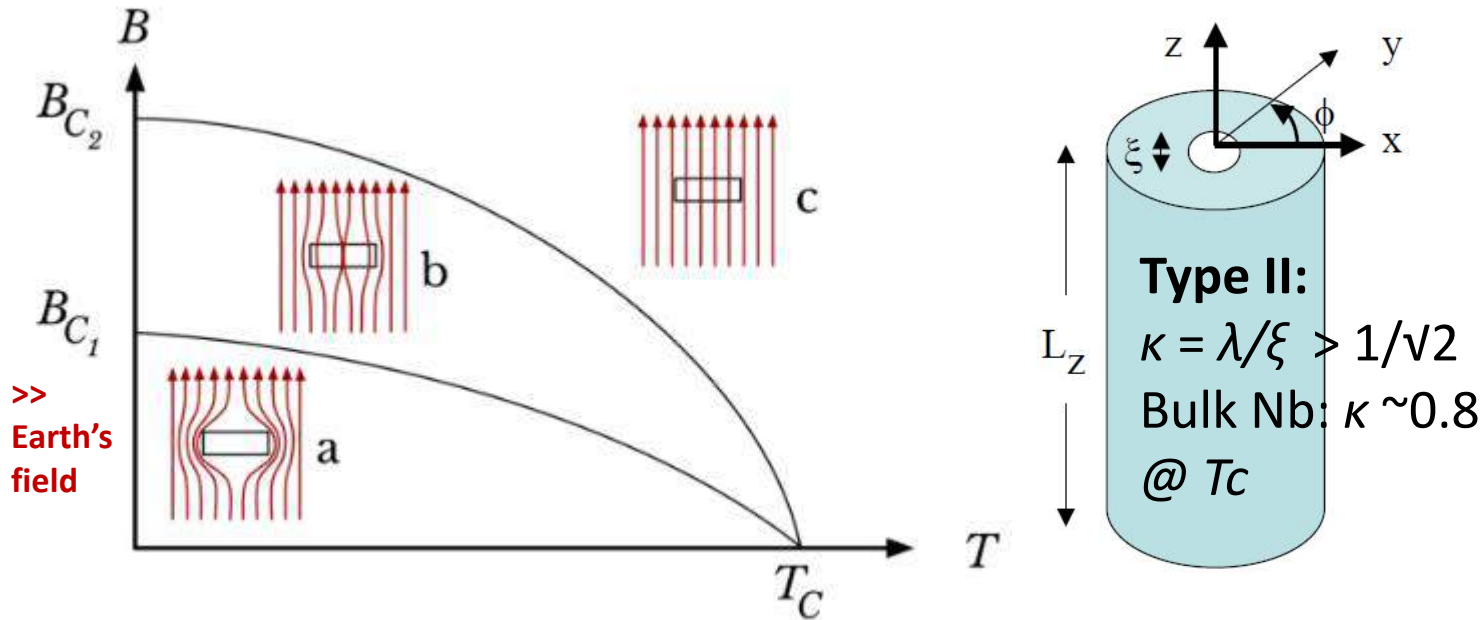


Thank You!



Manuel Castellanos-Beltran, Sam Benz, Paul Dresselhaus, David Olaya, Pete Hopkins

Trapped flux in Bulk Type II superconductors (e.g. Nb)



- Abrikosov (1957, Nobel 2003) - Type 2 Superconductors
- λ = London penetration depth, ξ = coherence length
- free of imperfections
- Imperfections can pin the flux

Dry cryostats: B Field from GM and Pulse Tubes NIST

GM Cryocooler



Cryogenic Fluxgate Magnetometer

